

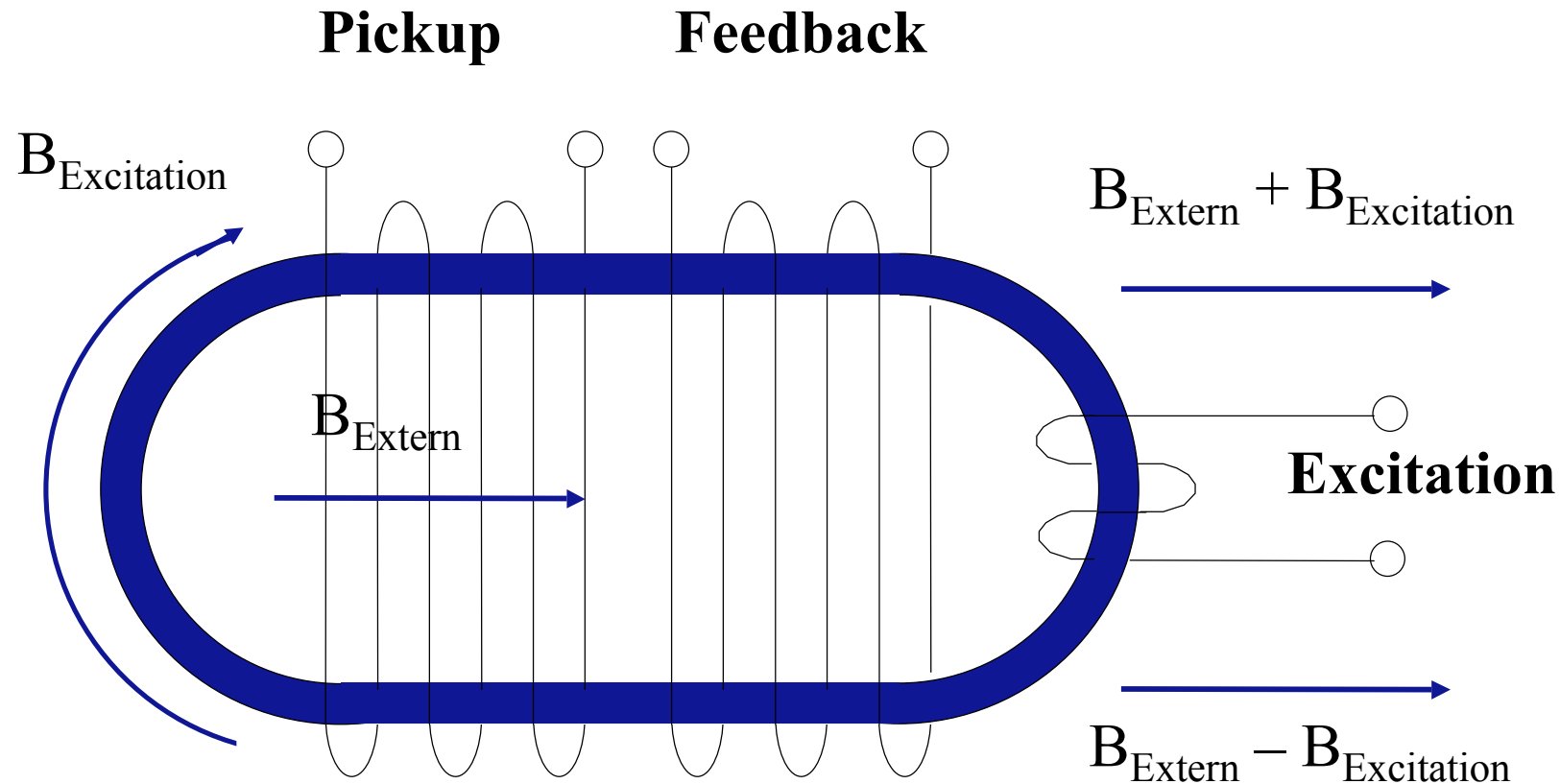


# *Fluxgate, Design and Calibration*

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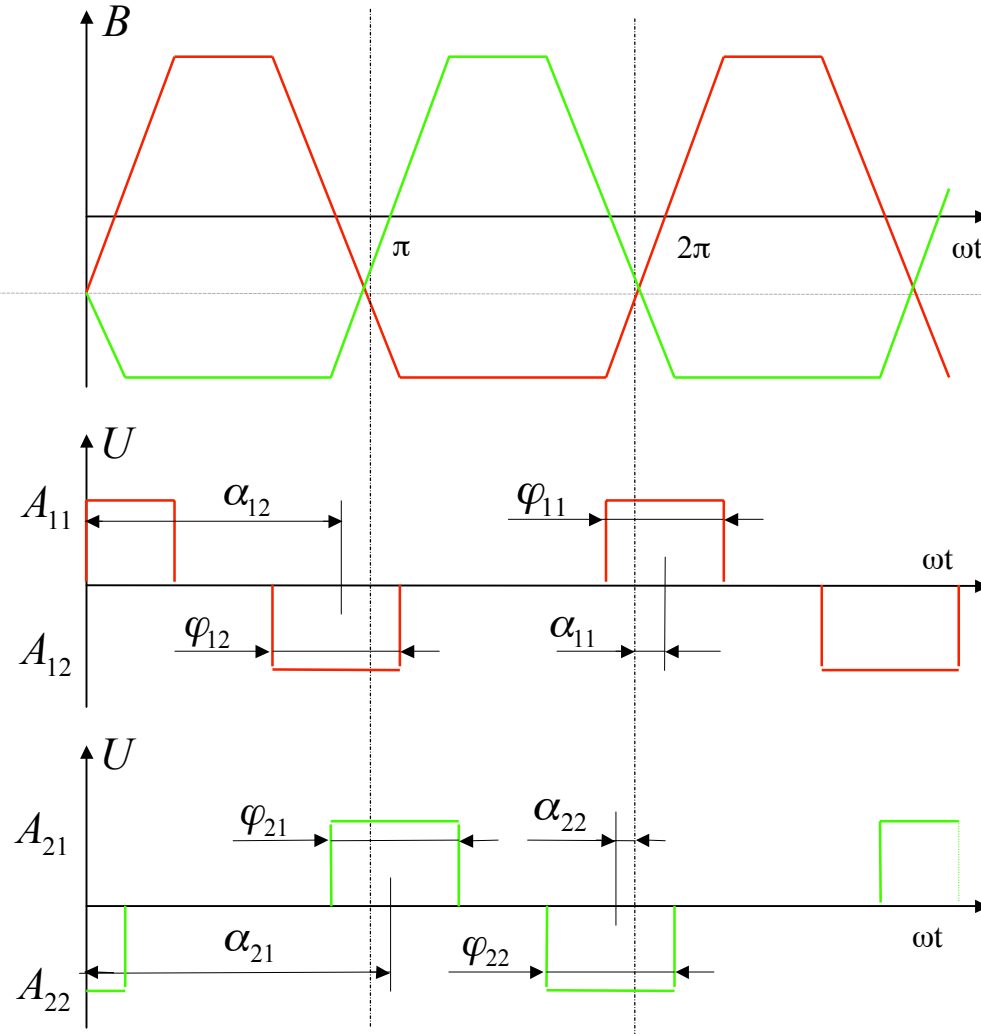
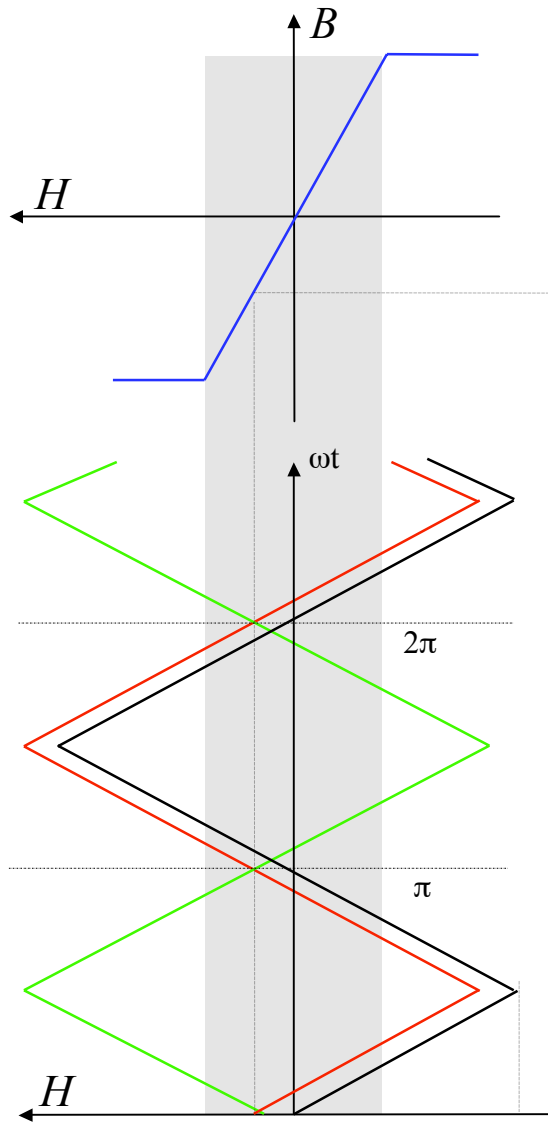
- Design of Fluxgate Magnetometer for Space application
  - Operation Principle
  - Sensor design
  - Electronics options
  
- Calibration of Fluxgate Magnetometer
  - On Ground Calibration:  
Parameter, Methods and Facilities
  - Inflight Calibration:  
Inputs, Methods and Procedure

# Operation Principle (1)



$$U = \frac{d\Phi}{dt} = \frac{d(nA\mu_0\mu_r(t)H(t))}{dt}$$

# Operation Principle (2)



# Operation Principle (3)

$$f(t) = \frac{2A_{11}}{\pi} \left\{ \frac{\varphi_{11}}{2} + \frac{\sin(\varphi_{11})}{1} \cos(\omega t + \alpha_{11}) + \frac{\sin(2\varphi_{11})}{2} \cos(2\omega t + 2\alpha_{11}) + \frac{\sin(3\varphi_{11})}{3} \cos(3\omega t + 3\alpha_{11}) + \dots \right\}$$

$$+ \frac{2A_{12}}{\pi} \left\{ \frac{\varphi_{12}}{2} + \frac{\sin(\varphi_{12})}{1} \cos(\omega t + \alpha_{12}) + \frac{\sin(2\varphi_{12})}{2} \cos(2\omega t + 2\alpha_{12}) + \frac{\sin(3\varphi_{12})}{3} \cos(3\omega t + 3\alpha_{12}) + \dots \right\}$$

$$+ \frac{2A_{21}}{\pi} \left\{ \frac{\varphi_{21}}{2} + \frac{\sin(\varphi_{21})}{1} \cos(\omega t + \alpha_{21}) + \frac{\sin(2\varphi_{21})}{2} \cos(2\omega t + 2\alpha_{21}) + \frac{\sin(3\varphi_{21})}{3} \cos(3\omega t + 3\alpha_{21}) + \dots \right\}$$

$$+ \frac{2A_{22}}{\pi} \left\{ \frac{\varphi_{22}}{2} + \frac{\sin(\varphi_{22})}{1} \cos(\omega t + \alpha_{22}) + \frac{\sin(2\varphi_{22})}{2} \cos(2\omega t + 2\alpha_{22}) + \frac{\sin(3\varphi_{22})}{3} \cos(3\omega t + 3\alpha_{22}) + \dots \right\}$$

$$A_{11} = \frac{B_{Sat}}{H_{Sat}} \frac{2\hat{H}_{Err}}{\pi}, \quad A_{12} = -\frac{B_{Sat}}{H_{Sat}} \frac{2\hat{H}_{Err}}{\pi}$$

$$\varphi_{ij} = \frac{\pi}{2\hat{H}_{Err}} H_{Sat}$$

$$\alpha_{11} = \frac{\pi}{2\hat{H}_{Err}} H_{Ext}, \quad \alpha_{12} = \pi - \frac{\pi}{2\hat{H}_{Err}} H_{Ext}, \quad \alpha_{21} = \pi + \frac{\pi}{2\hat{H}_{Err}} H_{Ext}, \quad \alpha_{22} = -\frac{\pi}{2\hat{H}_{Err}} H_{Ext}$$

$$f_1(t) = \frac{2A_{11}}{\pi} \sin(\varphi_{11}) \{ \cos(\omega t + \alpha_{11}) - \cos(\pi + \omega t - \alpha_{11}) + \cos(\pi + \omega t + \alpha_{11}) - \cos(\omega t - \alpha_{11}) \}$$

$$= 0$$

$$f_2(t) = \frac{A_{11}}{\pi} \sin(2\varphi_{11}) \{ \cos(2\omega t + 2\alpha_{11}) - \cos(2\pi + 2\omega t - 2\alpha_{11}) + \cos(2\pi + 2\omega t + 2\alpha_{11}) - \cos(2\omega t - 2\alpha_{11}) \}$$

$$= \frac{A_{11}}{\pi} \sin(2\varphi_{11}) \{ 2 \cos(2\omega t + 2\alpha_{11}) - 2 \cos(2\omega t - 2\alpha_{11}) \} = \frac{-4A_{11}}{\pi} \sin(2\varphi_{11}) \sin(2\alpha_{11}) \sin(2\omega t)$$



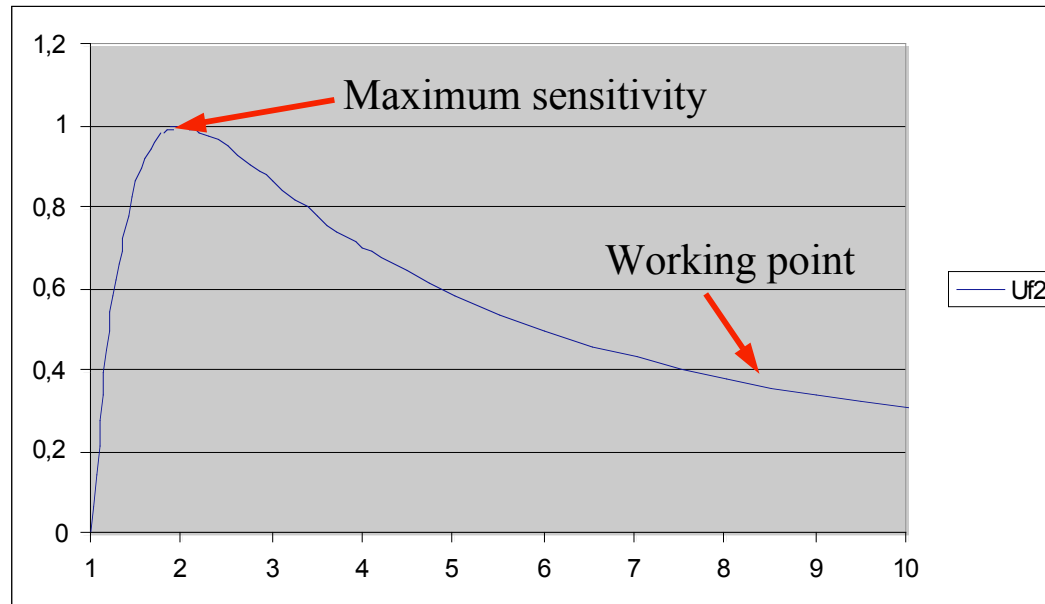
# Operation Principle (4)

$$f_2(t) = -4 \frac{B_{Sat}}{H_{Sat}} \frac{2\hat{H}_{Err}}{\pi^2} \sin\left(\pi \frac{H_{Sat}}{\hat{H}_{Err}}\right) \sin\left(\pi \frac{H_{Ext}}{\hat{H}_{Err}}\right) \sin(2\omega t)$$

für  $H_{Ext} \ll \hat{H}_{Err}$  gilt:

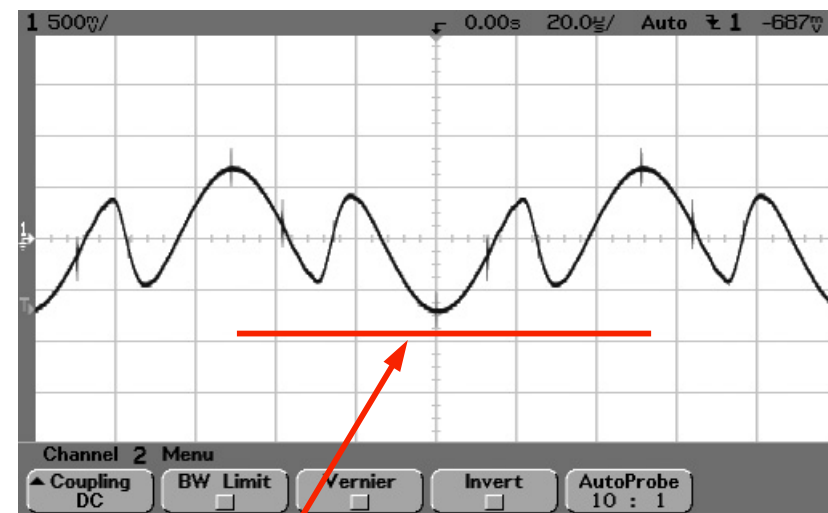
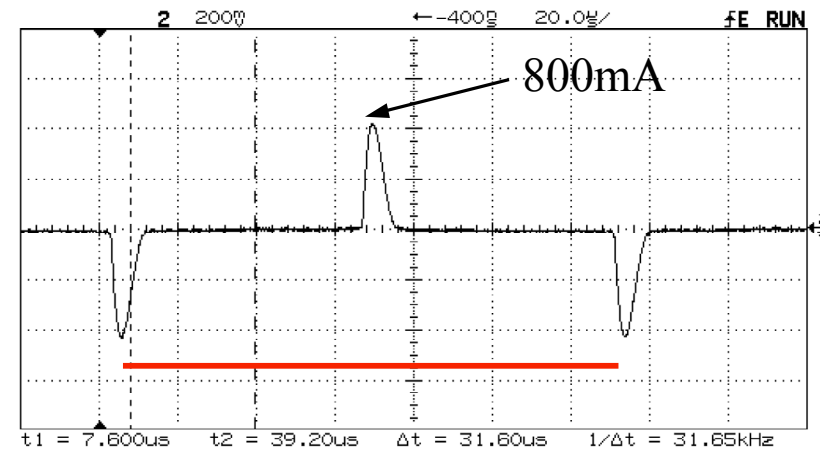
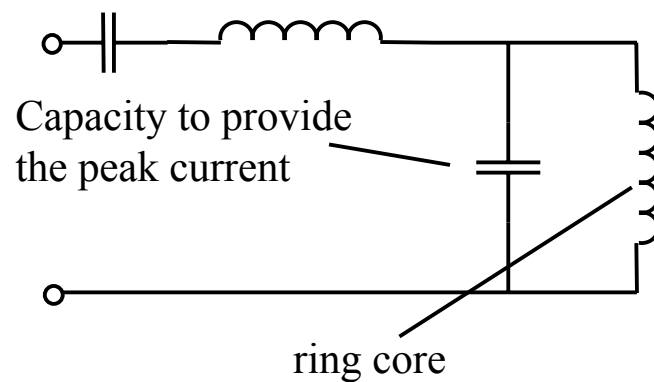
$$f_2(t) = -\frac{8}{\pi} \frac{B_{Sat}}{H_{Sat}} H_{Ext} \sin\left(\pi \frac{H_{Sat}}{\hat{H}_{Err}}\right) \sin(2\omega t)$$

$$U_2(t) = -\frac{8}{\pi} n A \omega \mu_0 \frac{B_{Sat}}{H_{Sat}} H_{Ext} \sin\left(\pi \frac{H_{Sat}}{\hat{H}_{Err}}\right) \sin(2\omega t)$$



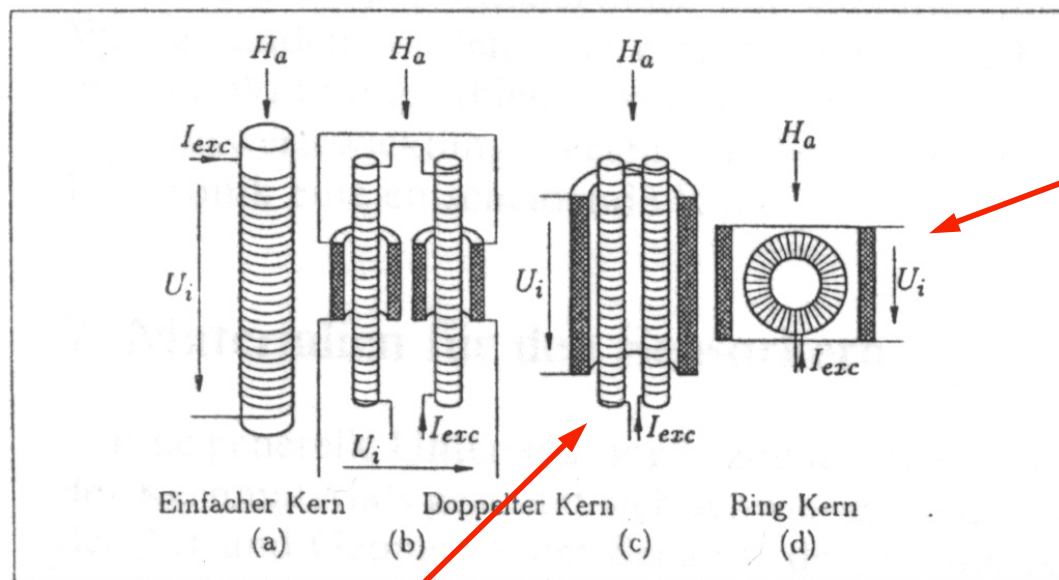
Amplitude  $U_{2f0}$  vs.  $H_{Err}/H_{Sat}$

- Excitation current is dominated by field dependent impedance of soft magnetic material
- Excitation frequency: 8-10kHz
- Symmetry: 70dB
- Power: 200mW, only 20% is consumed in sensor



# Types of Sensors

Bild 10: Parallele Sensortypen. (a) Einfacher Kern. (b) und (c) Doppelter Kern. (d) Ring-Kern.



- Double Rod
  - Förster
  - Rasmussen

☺ Low demagnetisation for external field

## ■ Ring Core

- Acuna
- Fornacon
- Afanasev
- Primdahl

☺ Low demagnetisation for excitation field

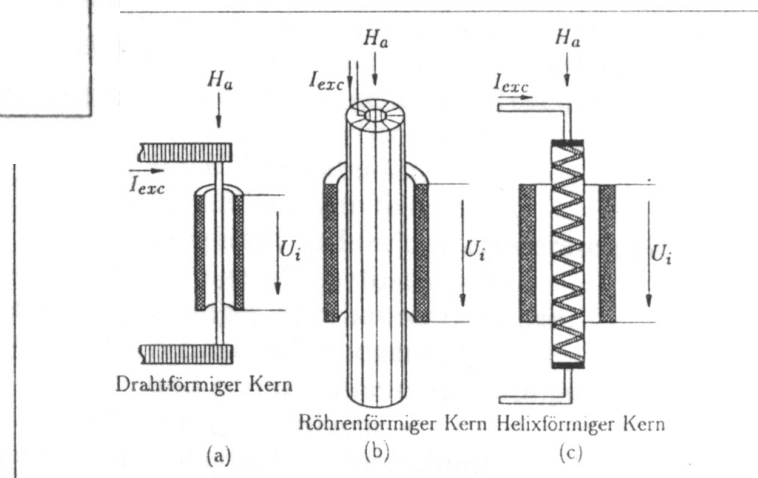
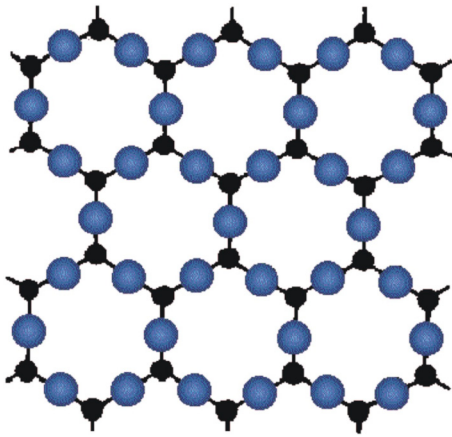


Bild 11: Orthogonale Sensortypen. (a) Kern aus ferromagnetischem Draht. (b) Röhrenförmiger Kern. (c) Helixförmiger Kern.

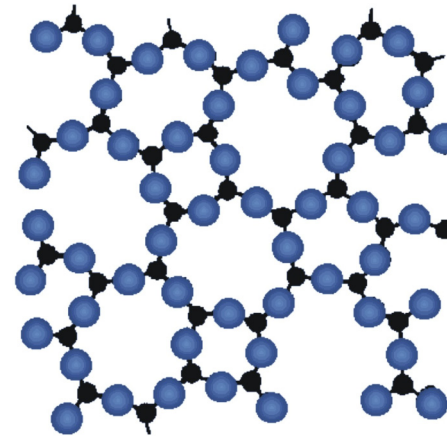
# *Magnetic Materials*



## ■ Crystalline Material

### *NiFe-Alloy*

- ☺ well processible
- ☺ high permeability  
(80 % Ni ca. 300 000)



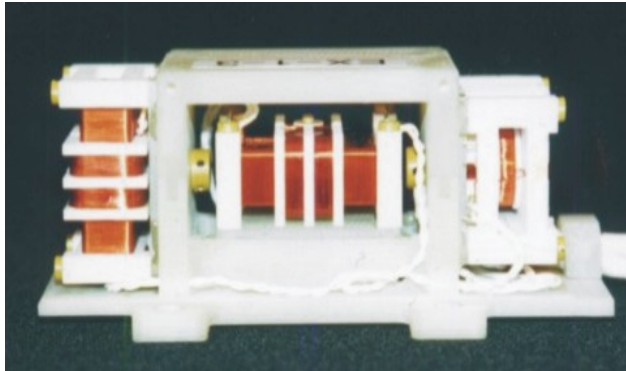
## ■ Amorphous Material

### *Fe- or Co-Alloy*

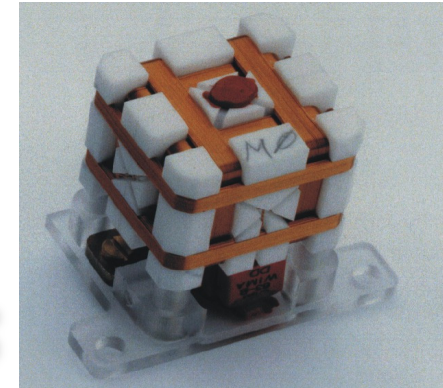
- ☺ Isotrop
- ☺ Low coercivity (low magnetisation losses)
- ☹ low Curie - temperature

- Selection of „best“ alloy
  - $\text{Fe}_{94-x}\text{Ni}_x\text{Mo}_6$      $x: 76 \dots 83$
- Manufacturing of soft-magnetic band
  - Hot and cold rolling up to  $10\mu\text{m}$  thickness
  - Cutting to 2mm width
- Manufacturing of ring cores
  - Accommodation of band on bobbin
  - Isolation by Magnesiumoxide
- Thermal treatment
  - Under vacuum or hydrogen atmosphere
  - temperature:  $900 \dots 1200^\circ\text{C}$

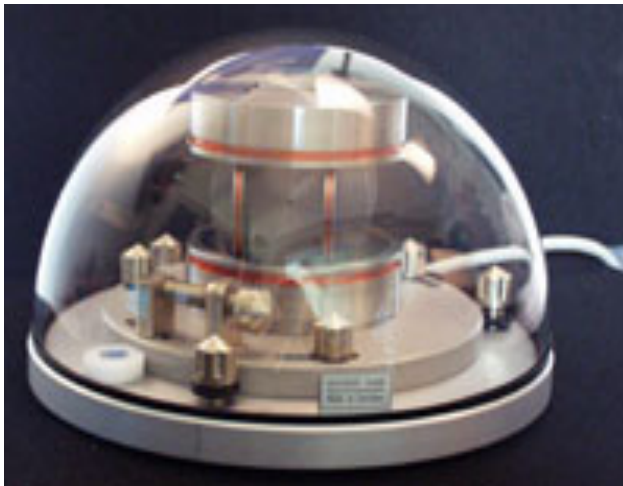
# *Examples of Sensors*



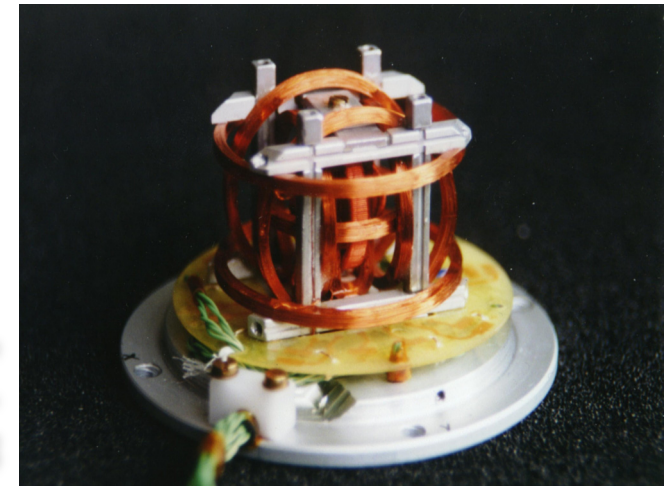
Mars96, Equator-S,  
Double Star,  
240g



Rosetta Orbiter, DS1,  
<50g, <10cm<sup>3</sup>



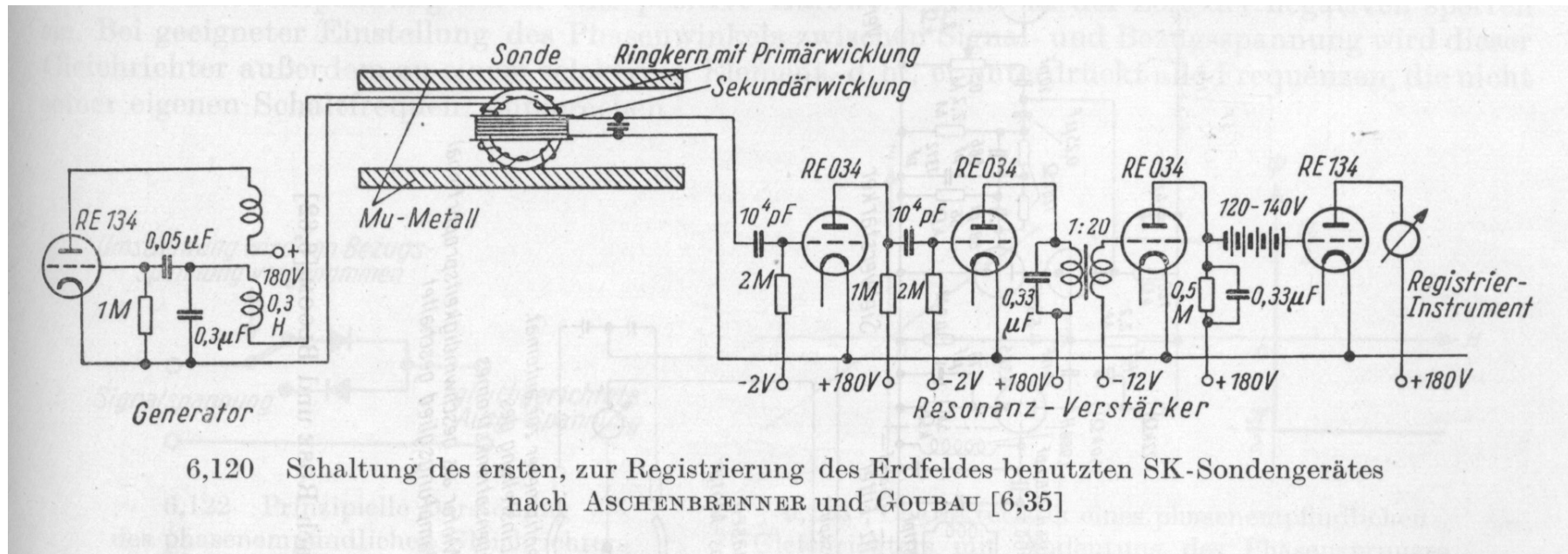
Observatories, MC,  
applied Geophysics  
3kg



Rosetta Lander, VEX,  
Themis, BepiColombo.  
<50g

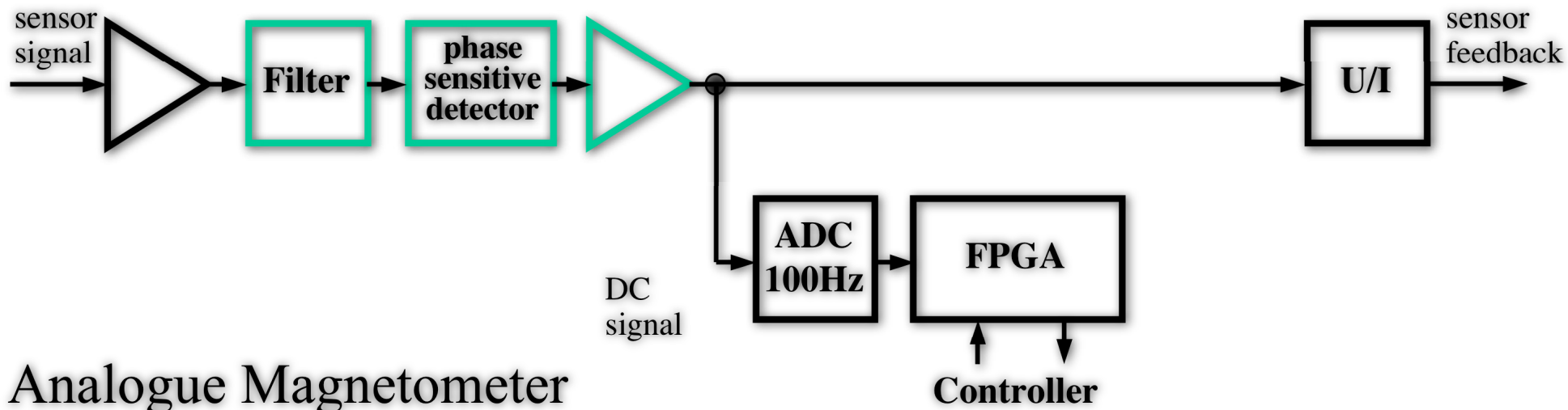


# First Fluxgate Magnetometers



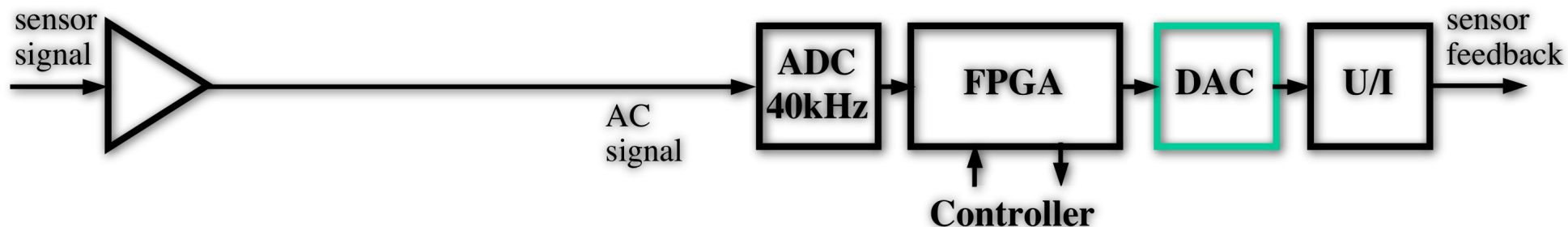
- Excitation Frequency: 700Hz
- Soft magnetic material: annealed wire
- Resolution: 0.3nT

# Signal Processing Options



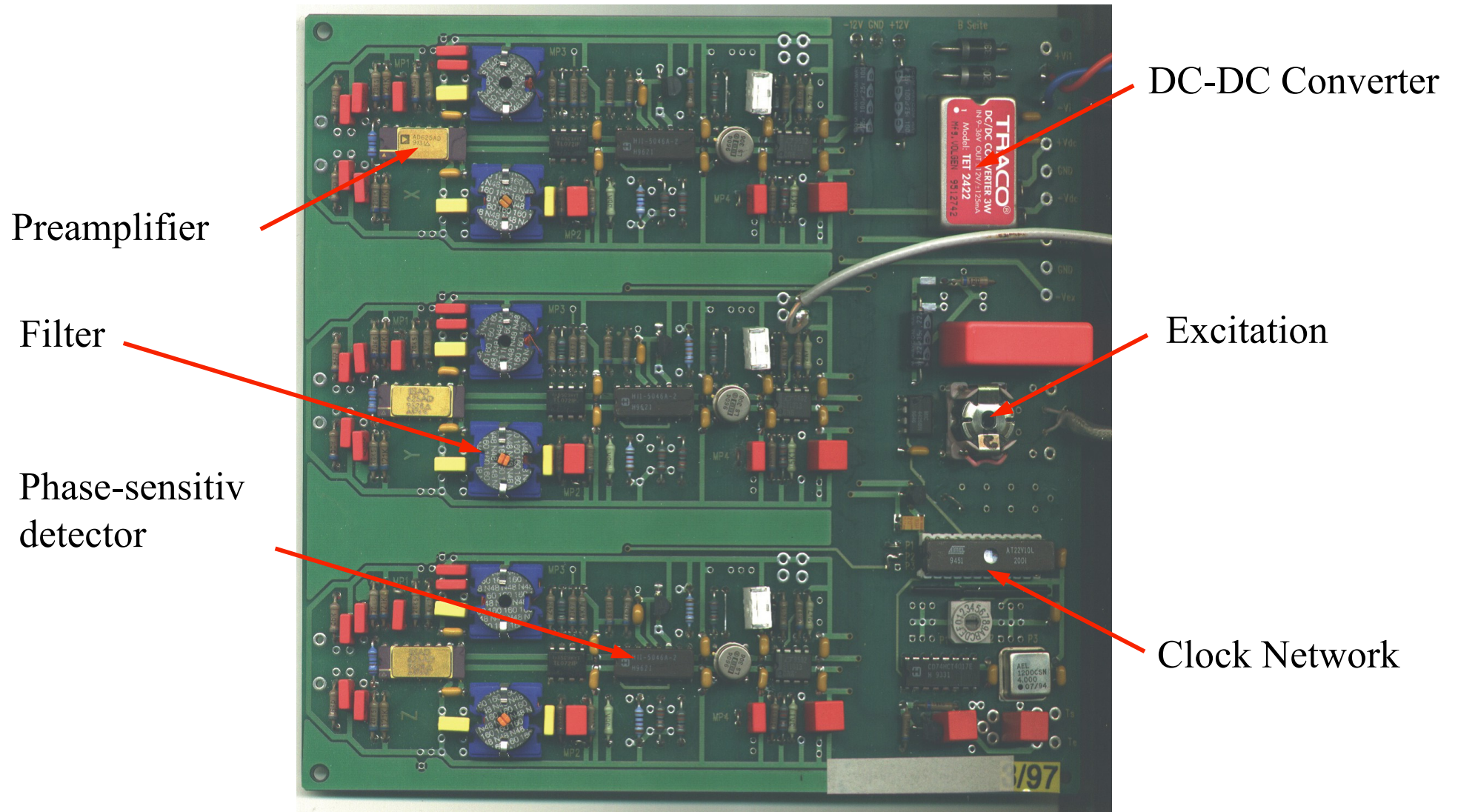
Analogue Magnetometer

## Digital Magnetometer

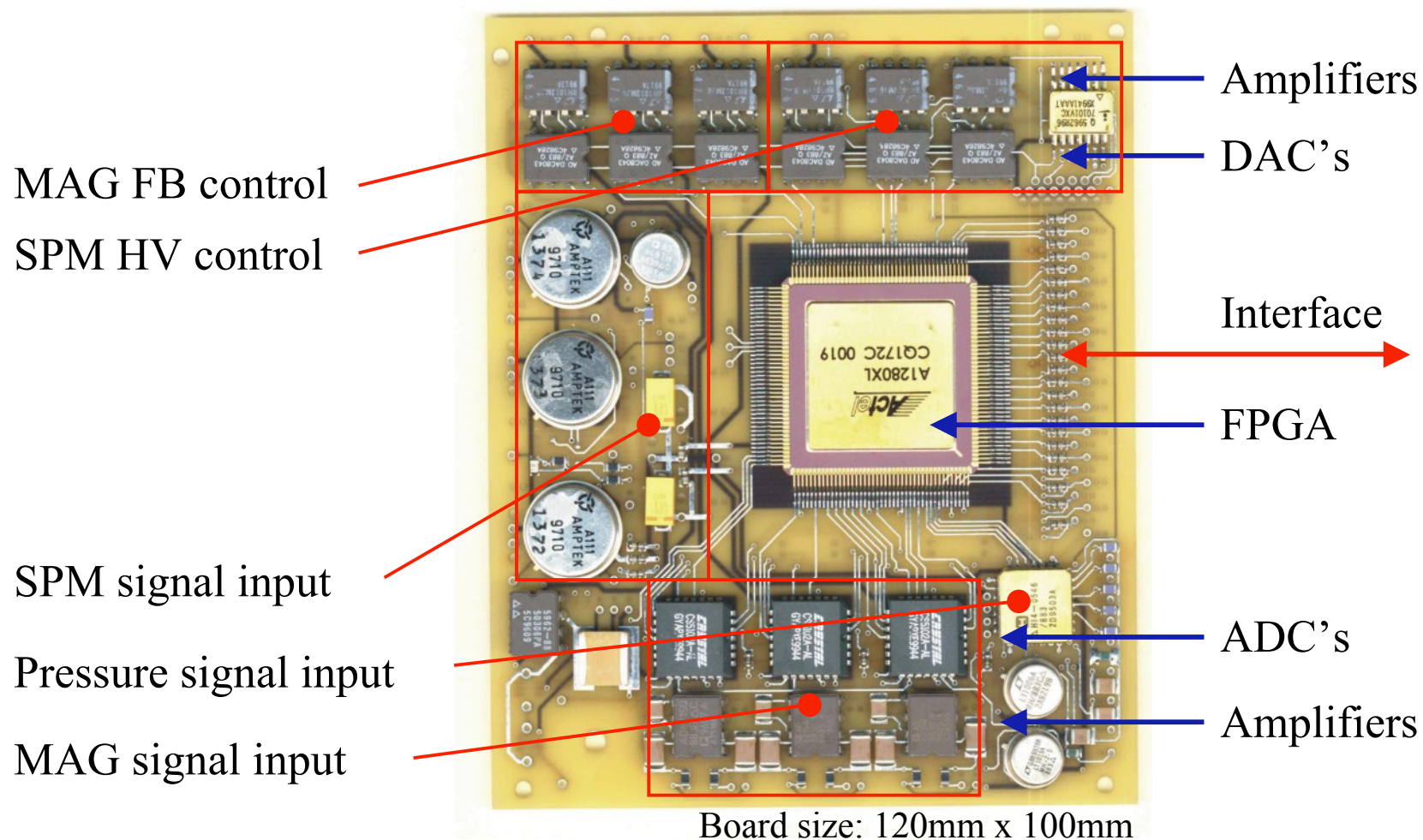




# *Example Analogue FGM*



## ROMAP: Magnetometer (MAG) + Plasmamonitor (SPM)





# *Fluxgate Design References*

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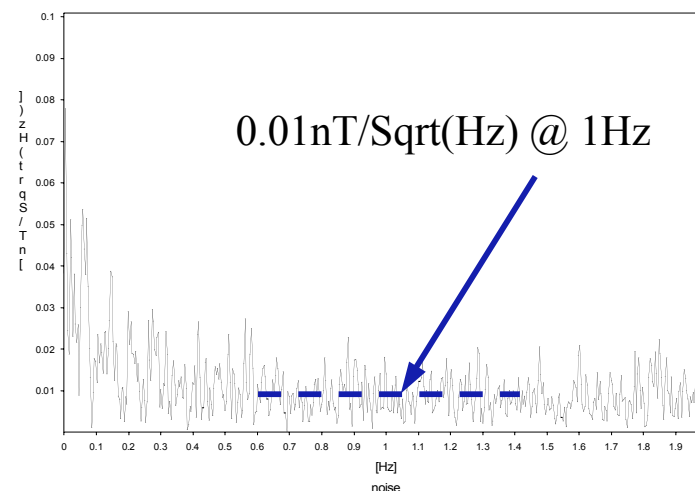
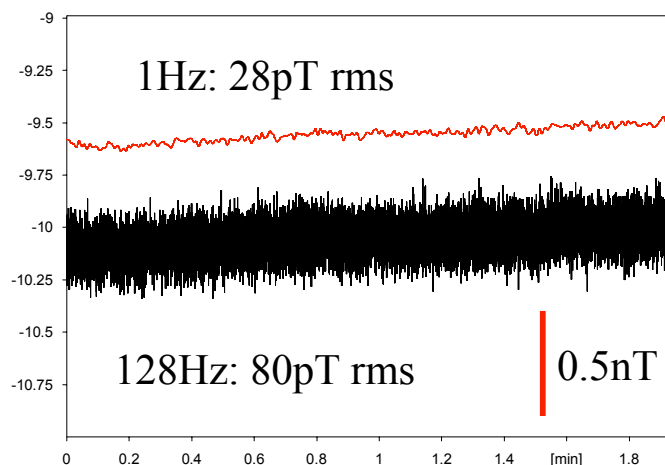
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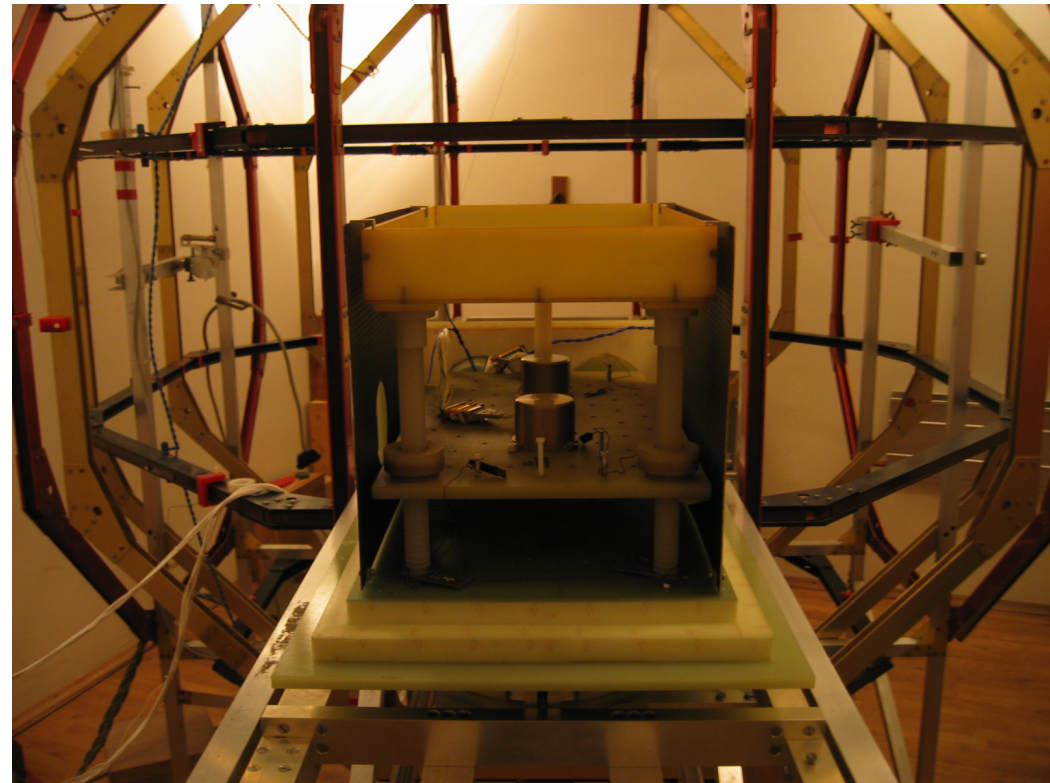
# Calibration Parameters

Parameter	Error Source	typ. value
Offsets (output at zero field) depends on time and temp.	asymmetry of sensor and excitation offsets of DC electronics, ADC ...	0-10nT 0.2nT/day; 0.05nT/°C
Scale value depends on temperature	scale value shall depends on feedback circuitry only – current source & feedback coil system	$10^{-4}$ 1-30ppm/°C
Non linearity	at low fb factors: 2f0 non linearity at high fb factors: feedback circuitry non linearity	$10^{-4}$
Orthogonality	vector compensated: depends on fb coil system single sensors depends on ringcore /pick up coil	$10^{-4}$
Bandwidth	frequency behavior depends on analogue or digital filter. Has to be switched with telemetry rate	
Noise	should be ringcore property (no contribution of electronics), depends on frequency	10pT/Sqrt(Hz) at 1Hz



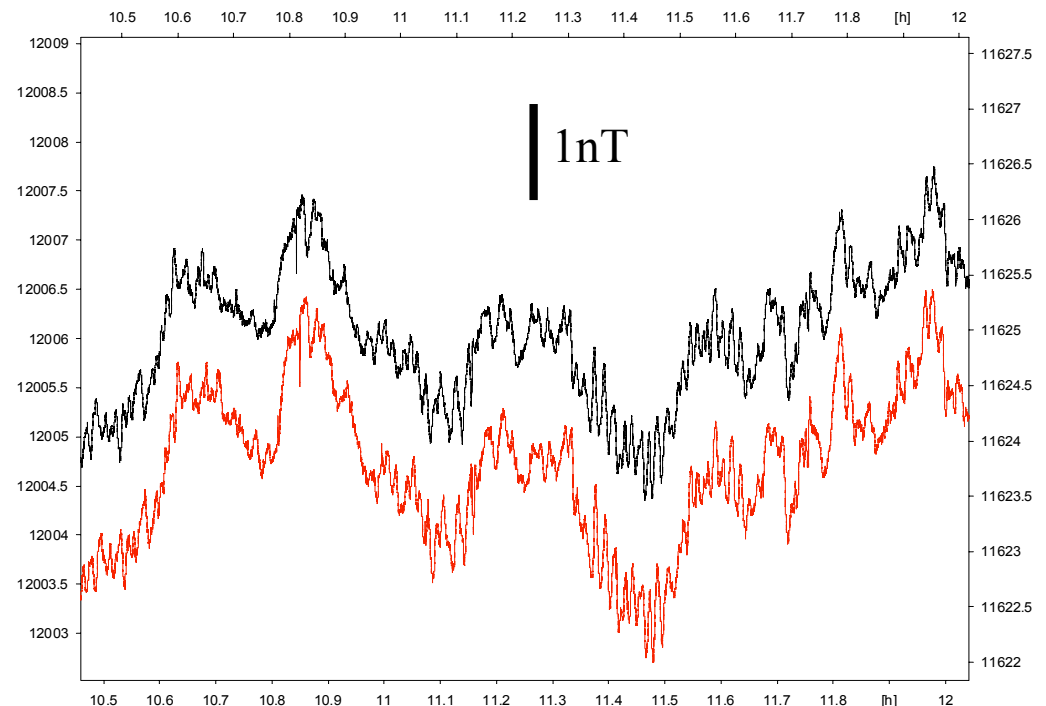
# *Ground Calibration Methods (1)*

- Using well controlled, synthesized test fields
  - Sensor placed in coil systems
  - quiet environment required, Earth field variations as well as technical disturbances under control
  - Precise measurement / setting of coil currents
  - Air conditioning necessary
  - Calibration of coil system by (absolute) scalar magnetometer possible
  - Example: Magnetsrode close to Braunschweig



# Ground Calibration Methods (2)

- Using the Earth field measured by a independent magnetometer
  - Sensor placed on a stable (non magnetic) pillar
  - Registration of Earth field in parallel to standard observatory instruments (or between flight models)
  - Noise can be checked by short term registration of pulsation
  - Drift can be checked after days-weeks registration
  - Most of the observatories offer this service



# Ground Calibration Methods (3)

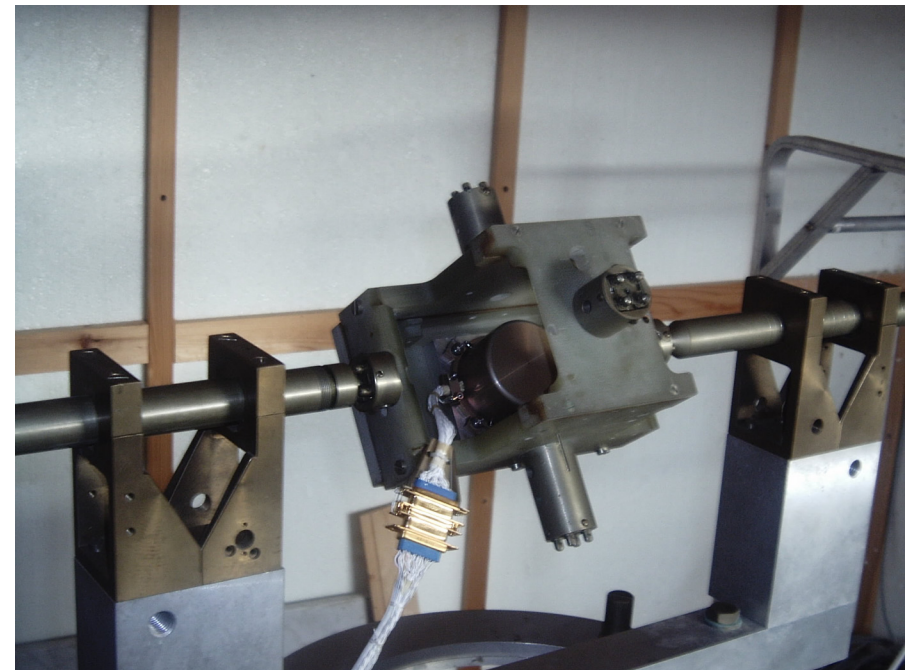
- Using „zero“ fields
  - Sensor placed in ferromagnetic can which shields the Earth field
  - Noise and offset stability can be checked
  - If sensor can be rotated offsets in components perpendicular to rotation can be determined
  - Example: transportable mu-metal can, equipped with temperature chamber (Graz)





# *Ground Calibration Methods (4)*

- Using a controlled motion of the sensor in the Earth field
  - Rotation about a well defined axis perpendicular to the Earth field
  - Misalignment rotation and magnetic axis results in a sine function
  - Misalignment can be absolutely derived by amplitude and phase
- Using an arbitrary motion of the sensor in the Earth field
  - Assuming a linear transfer function, 9 of 12 elements (offset, scale values, orthogonality) can be derived by comparison with the Earth field magnitude





- Aim of inflight calibration
  - Determination of 12 elements of transformation  $\mathbf{B}_M$  to  $\mathbf{B}_{SC}$
  - Assumption: transformation is linear
  - $\mathbf{M}_{Cal}$  Calibration Matrix;  $\mathbf{O}_{Cal}$ : Calibration Offset

$$\mathbf{M}_{Cal} (\mathbf{B}_M - \mathbf{Z}_{Cal}) = \mathbf{B}_{SC}$$

- Calibration Matrix  $\mathbf{M}_{Cal}$  shall be split up in three quantities
  - **S**: represents **scale values** with elements in the main axis
  - **O**: represents the **non orthogonality** (triangular matrix)
  - **R**: represents the orientation of the orthogonal system versus S/C system (rotation matrix)

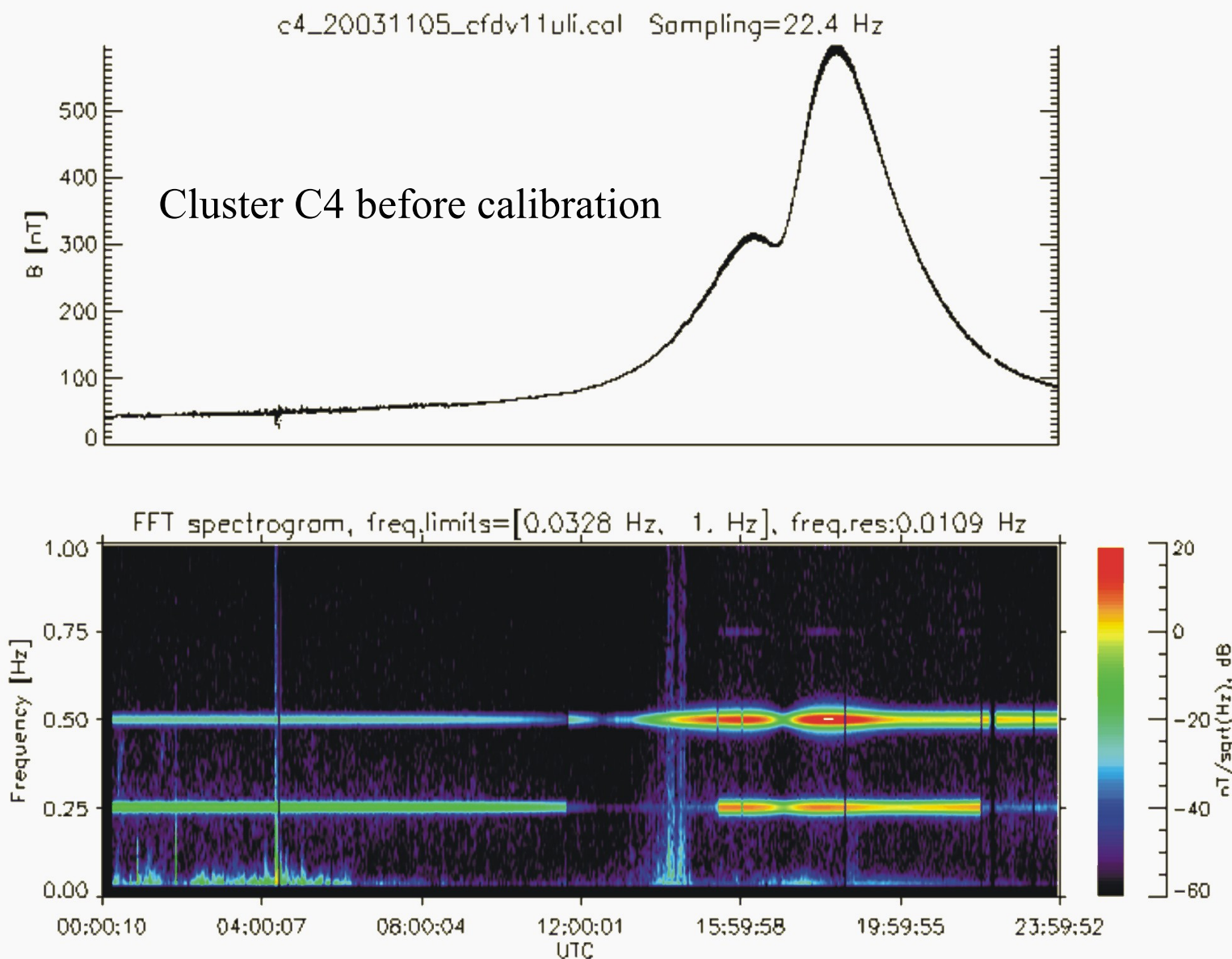
$$\mathbf{O} \mathbf{S} (\mathbf{B}_M - \mathbf{Z}_{Cal}) = \mathbf{R} \mathbf{B}_{SC}$$

- Calibration methods are based on the following relevant inputs
  - No spin and double spin tone in field magnitude
  - Field properties (Earth field model, Alfven waves, ...)
  - Knowledge of preflight calibration and MC results
  - Experiment specifics, mode and housekeeping information
  - Independent field measurements
  - Inter-calibration: using spacecraft comparisons ( $B_1=B_n$ ,  $\text{Rot}B=0$ ,  $\text{Div}B=0$ ) to level all instruments errors

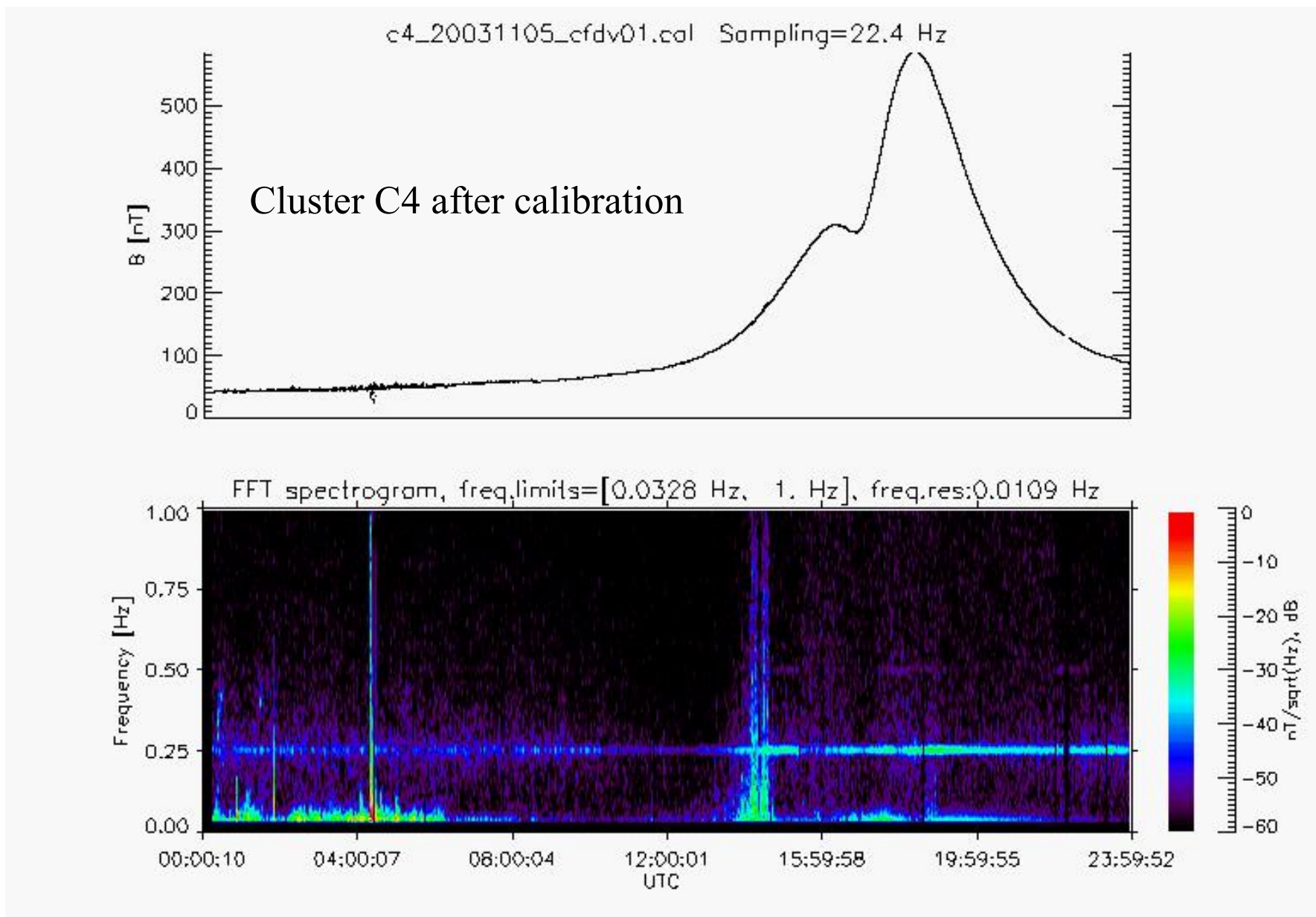
## Field magnitude has to be independent from sensor motion

$$\frac{\partial \left( \left\| \mathbf{O} \quad \mathbf{S} \quad (\mathbf{B}_M - \mathbf{Z}_{Cal}) \right\| \right)}{\partial (\mathbf{R})} \stackrel{!}{=} 0$$

- Conditions:
  - $\mathbf{B}_{\text{external}} \rightarrow \text{constant}$
  - $\mathbf{R} = R(\varphi, \psi, \vartheta) \rightarrow \text{variable}$
  - $\mathbf{O}, \mathbf{S}, \mathbf{Z}_{Cal} \rightarrow \text{doesn't depend on time and external field}$
- Effects assuming S/C rotation as motion
  - spin and double spin tone in field magnitude (4 equations)
  - All three angle of orthogonality affected
  - Offsets and scale values perpendicular to rotation axis affected



Calibration - in flight - methods (3) - example



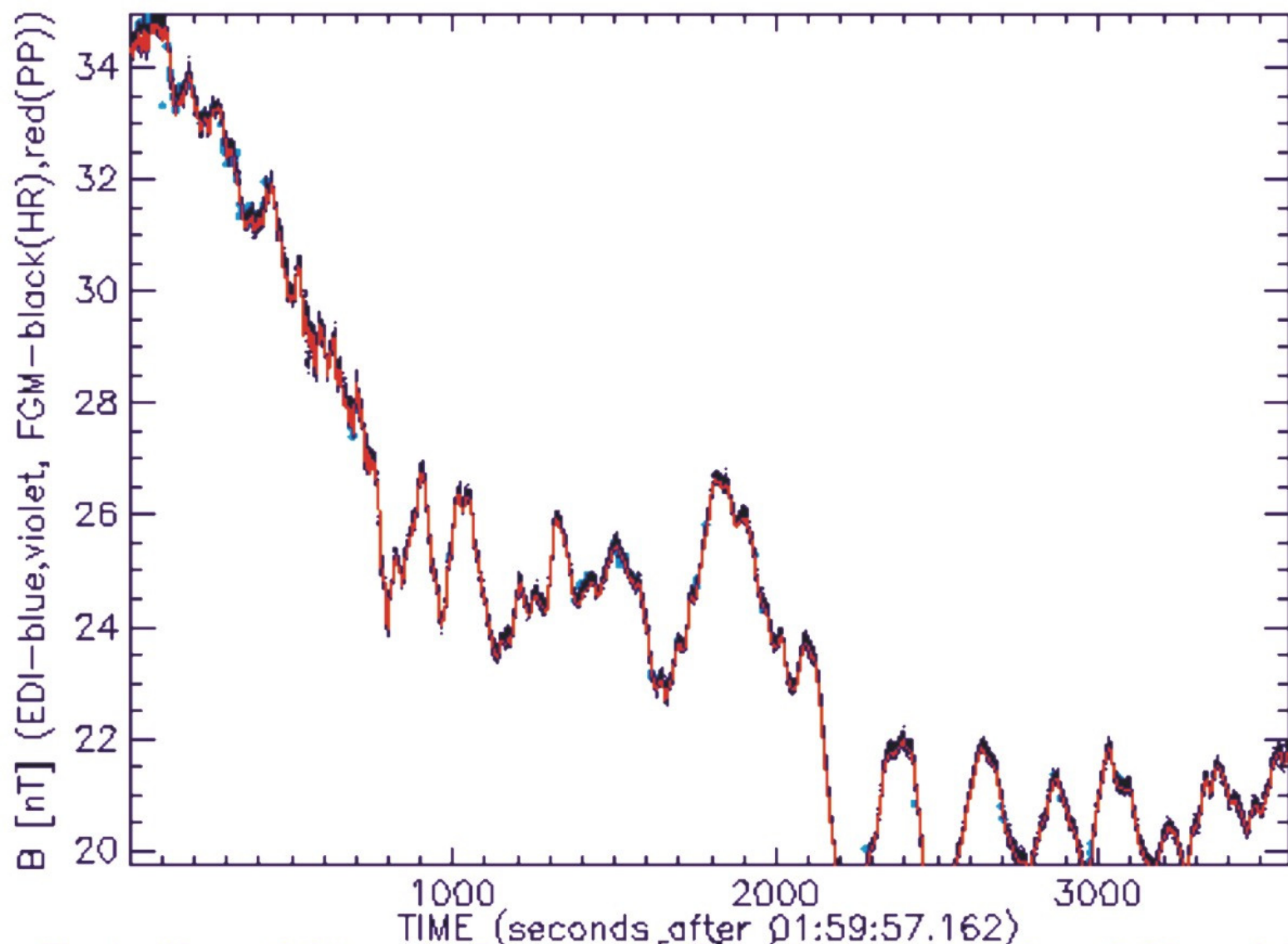
Calibration - in flight - methods (3) - example

**Field magnitude has to be equal to the magnitude measured by an independent (scalar) magnetometer**

$$|\mathbf{O} \quad \mathbf{S} \quad (\mathbf{B}_M - \mathbf{Z}_{Cal})| = |\mathbf{R} \quad \mathbf{B}_{SC}| \stackrel{!}{=} \mathbf{B}$$

- Conditions:
  - $\mathbf{B}_{\text{external}}$  → shall be variable
  - $\mathbf{R}$  → can be arbitrary
  - $\mathbf{O}, \mathbf{S}, \mathbf{Z}_{Cal}$  → doesn't depend on time and external field
- Examples
  - Proton magnetometer on board satellites investigating the Earth magnetic field (low orbits, e.g. Magsat, Oersted, Champ)
  - EDI onboard Equator-S, Cluster and MMS





Final offs: 0.09 -2.35 -1.08 [nT] (d\_offs: -0.10 -0.09 -0.33)

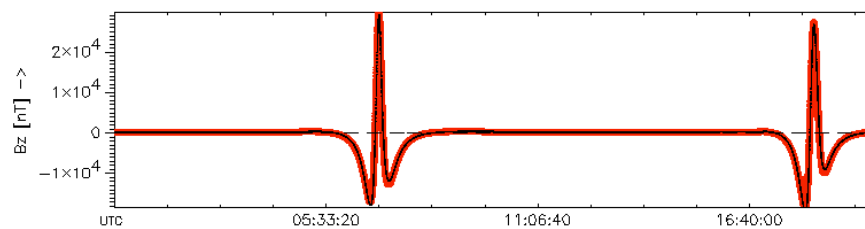
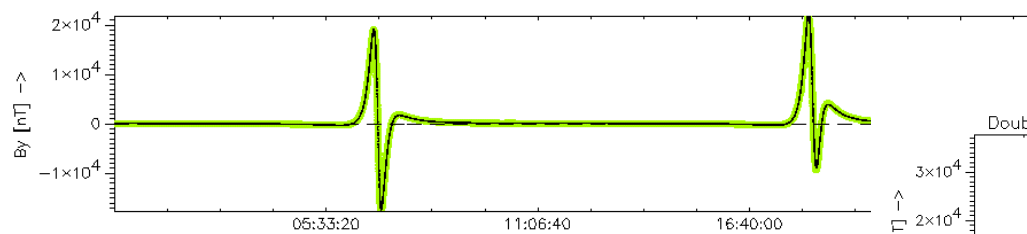
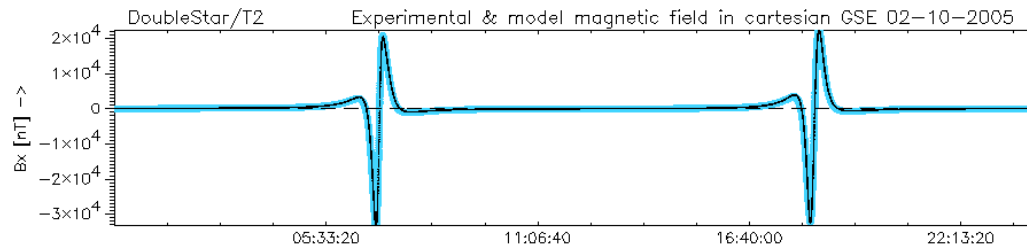
Calibration - in flight - methods (2) - example

## Measured field vector has to be in agreement with known physical features

$$f(\mathbf{O}, \mathbf{S}, (\mathbf{B}_M - \mathbf{Z}_{Cal})) \stackrel{!}{=} \text{Expectation}$$

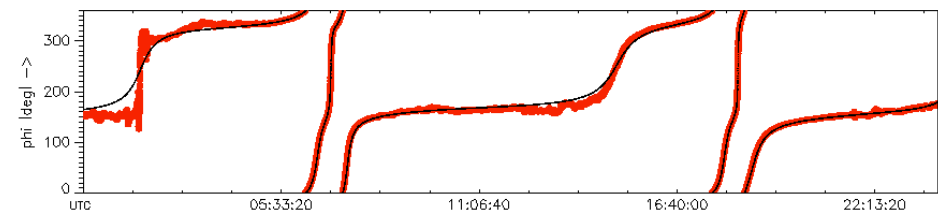
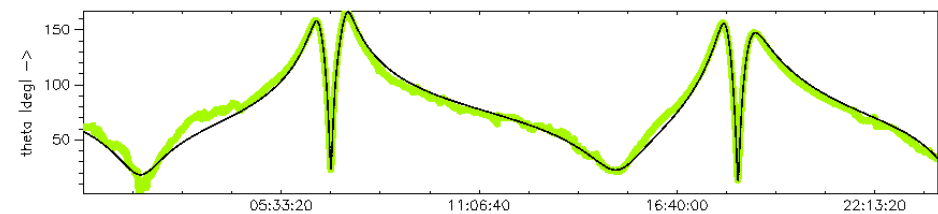
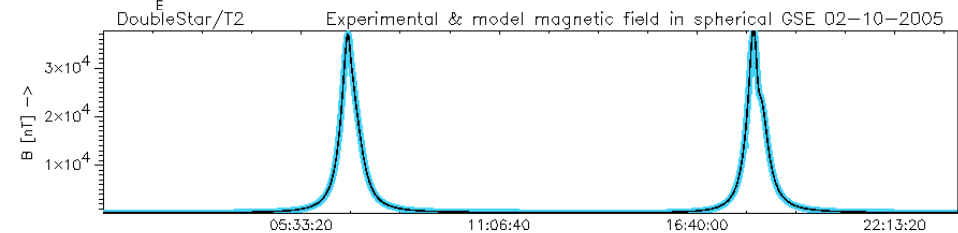
- Conditions:
  - $\mathbf{B}_{\text{external}}$  → shall be variable
  - $\mathbf{R}$  → can be arbitrary
  - $\mathbf{O}, \mathbf{S}, \mathbf{Z}_{Cal}$  → doesn't depend on time and external field
- Examples
  - In agreement with Earth field models
  - Alfven waves in solar wind
  - Divergence  $\mathbf{B}=0$ , Cavity of Comets ...





Calibration file name: T2.fgmodel

MODEL = IGRF + Tayganenko\_B9, kp = 1, Fri Oct 21 08:17:56 2005 by eg

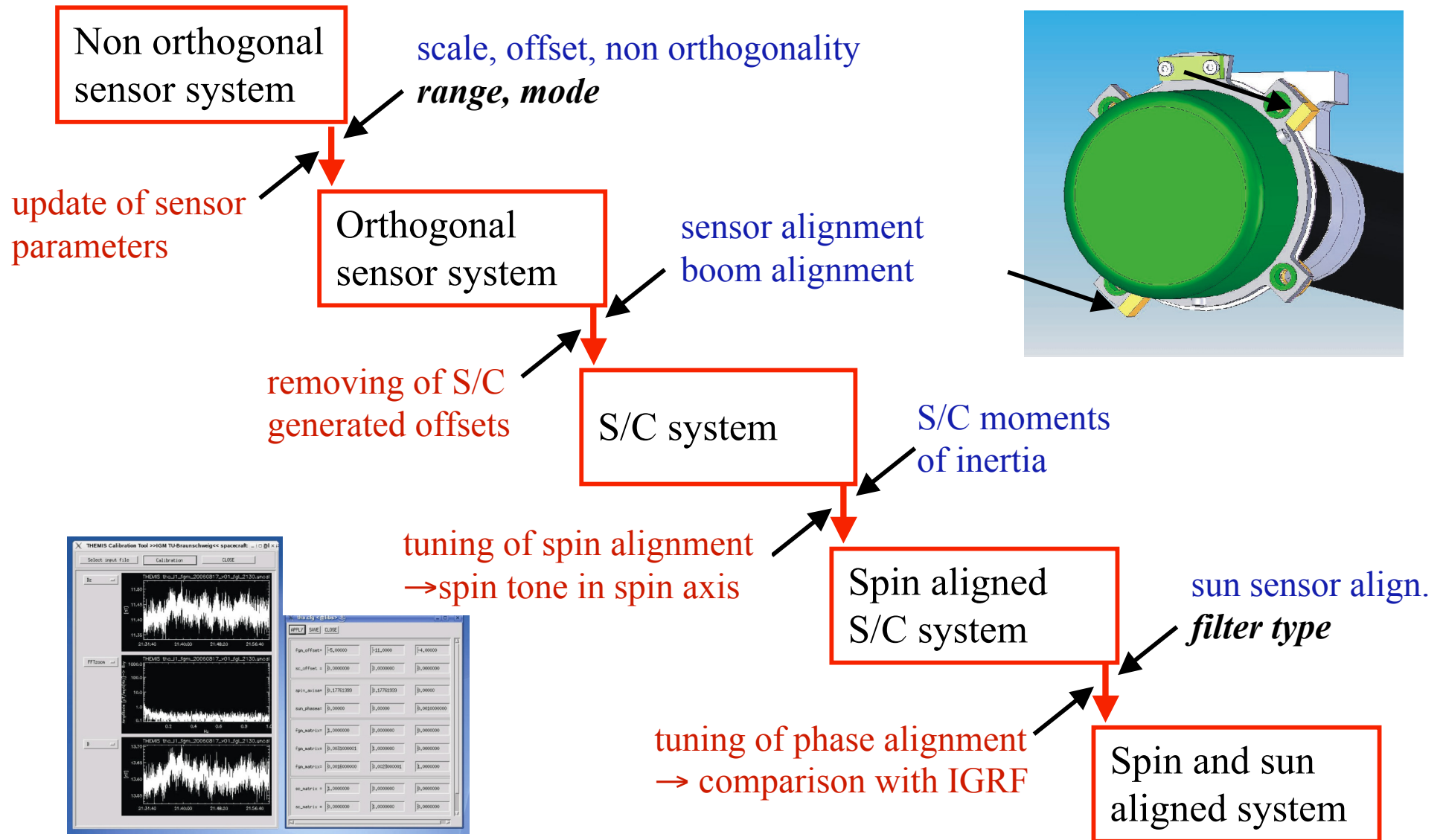


Calibration file name: T2.fgmodel

MODEL = IGRF + Tayganenko\_B9, kp = 1, Fri Oct 21 08:17:56 2005 by eg

Calibration - in flight - methods (3) - example

# Calibration Procedure





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- Visualisation and Calibration of Ground Calibration Data
  - Plot of uncalibrated data
  - 9 parameter Fit on known (constant) field magnitude
  - Plot of calibrated data
  - Check of sensitivity of method versus parameter
- Visualisation and Calibration of Cluster data
  - Plot of uncalibrated data
  - 4 parameter Fit on unknown constant field magnitude
  - Plot of calibrated data
  - Introducing of calibration errors and checking of influence on spin and double spin tone in magnitude